



CEP Stabilization MEDEA Webinar

Fabian Lücking

Spectra Physics Vienna

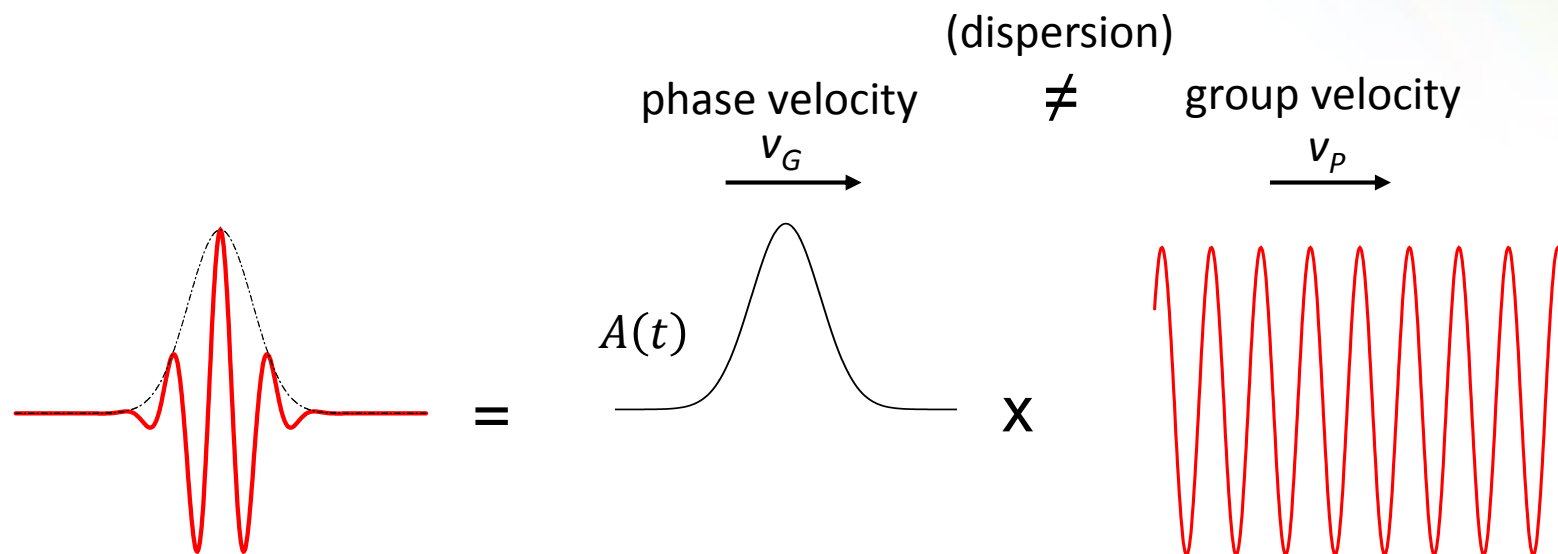
2016-03-16

1. The Carrier-Envelope Phase and its Changes
 - Time/Frequency picture
2. f_{ceo} – Measuring CEP Change
 - Linear method
 - Self-referencing
 - Interferometer types
3. From Random Change to Stable Change: Stabilizing f_{ceo}
 - What handle to turn?
 - Some less obvious handles
 - A word on residual noise characterization
4. From nJ to mJ – CEP stabilization in Amplifiers
 - Measuring the CEP of a single pulse
 - Nyquist's curse and how to live with it
5. Outlook
 - Current 'hot topics' in CEP
 - How good is good enough?

Introduction

THE CEP AND ITS CHANGES

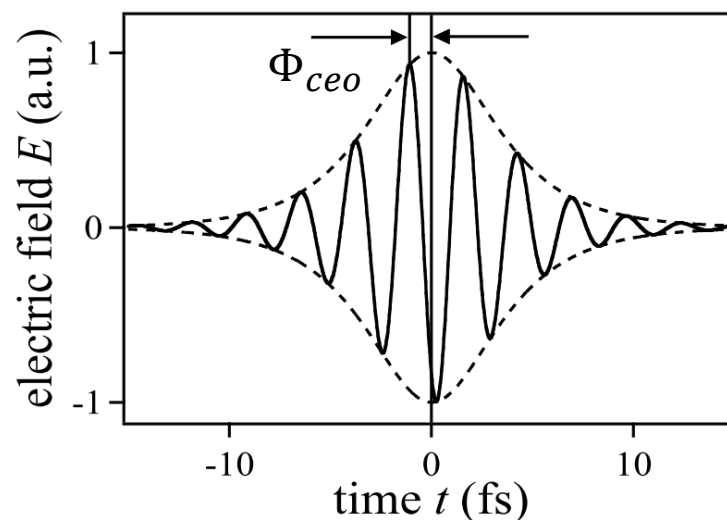
The Carrier-Envelope Phase



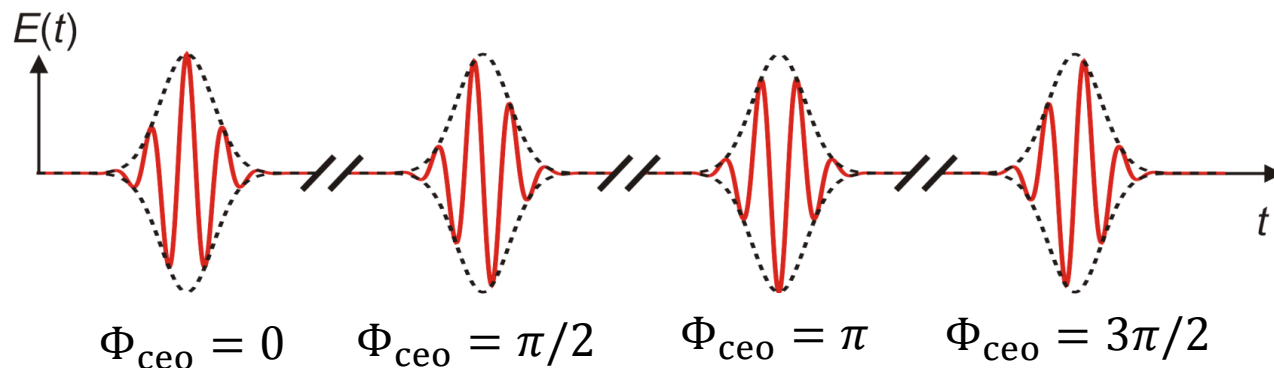
The CEP, Φ_{ceo} is

- the property of a **single pulse**
- unambiguous within $[0, 2\pi]$
- a function of time through
 - Dispersion
 - Nonlinearity
 - Geometry
 - ...

$$E(t) = A(t) \exp(i\omega_0 t + i\Phi_{ceo})$$



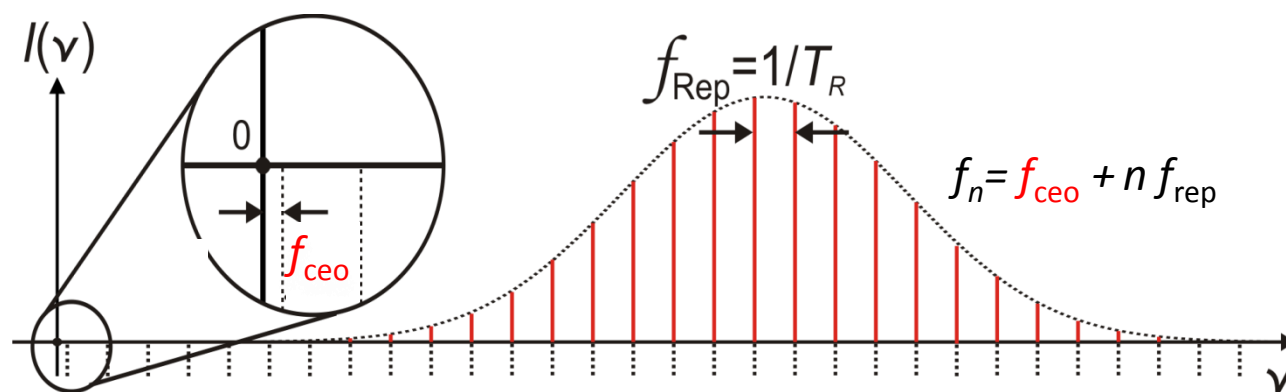
Output of a mode-locked oscillator



Time domain: $\Delta\Phi$

- ns pulse spacing T_{rt}
- Intracavity effects (dispersion, nonlin...) determine **roundtrip phase change $\Delta\Phi_{ceo}$**
- Can't measure Φ_{ceo}

$$T_{rt} = 1/f_{rep}; \Delta\Phi_{ceo} = 2\pi \frac{f_{ceo}}{f_{rep}} \quad \downarrow \text{Fourier transform}$$



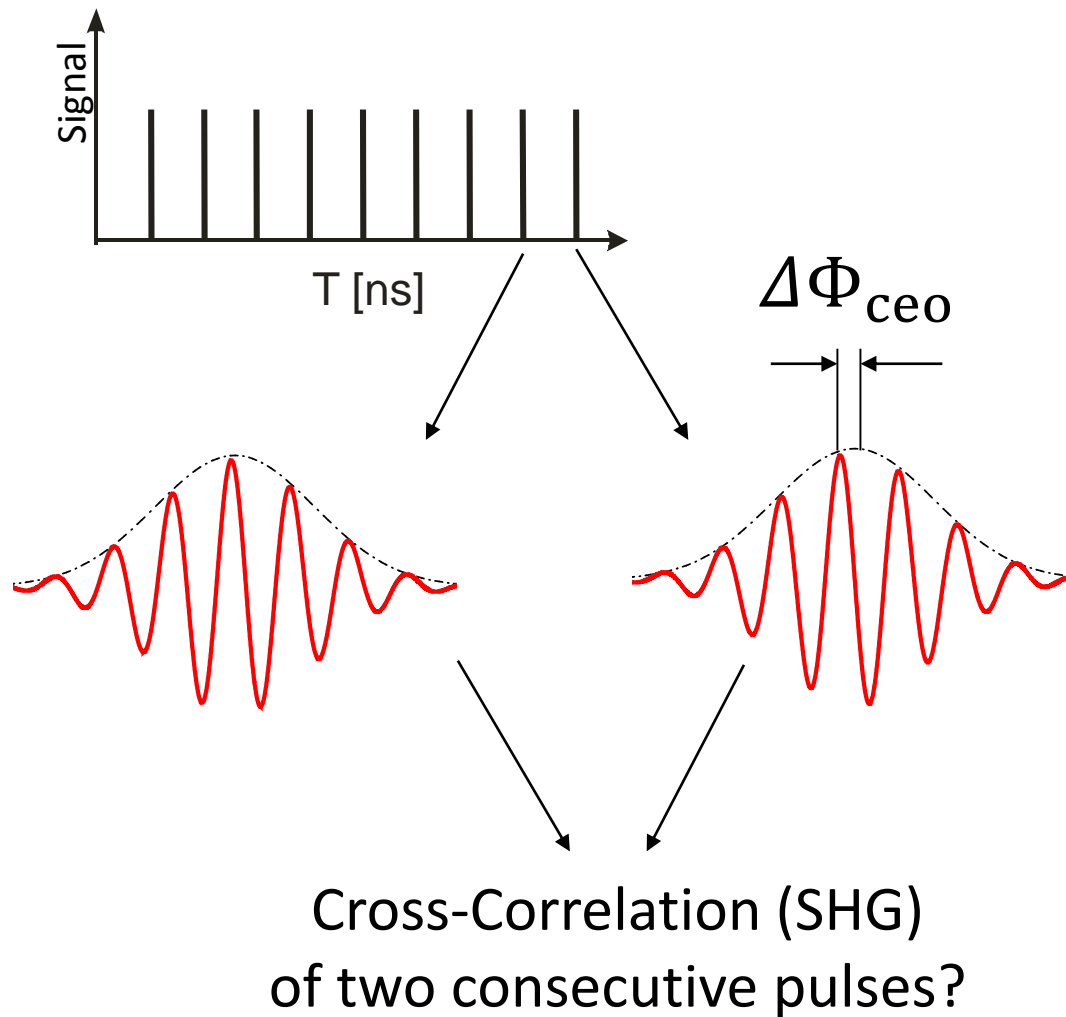
Frequency domain: f_{ceo}

- Frequency comb, determined by two parameters:
- **Repetition rate f_{rep}**
- **Comb offset f_{ceo}**
- Optical frequency of each line in spectrum
 $f_n = n f_{rep} + f_{ceo}$

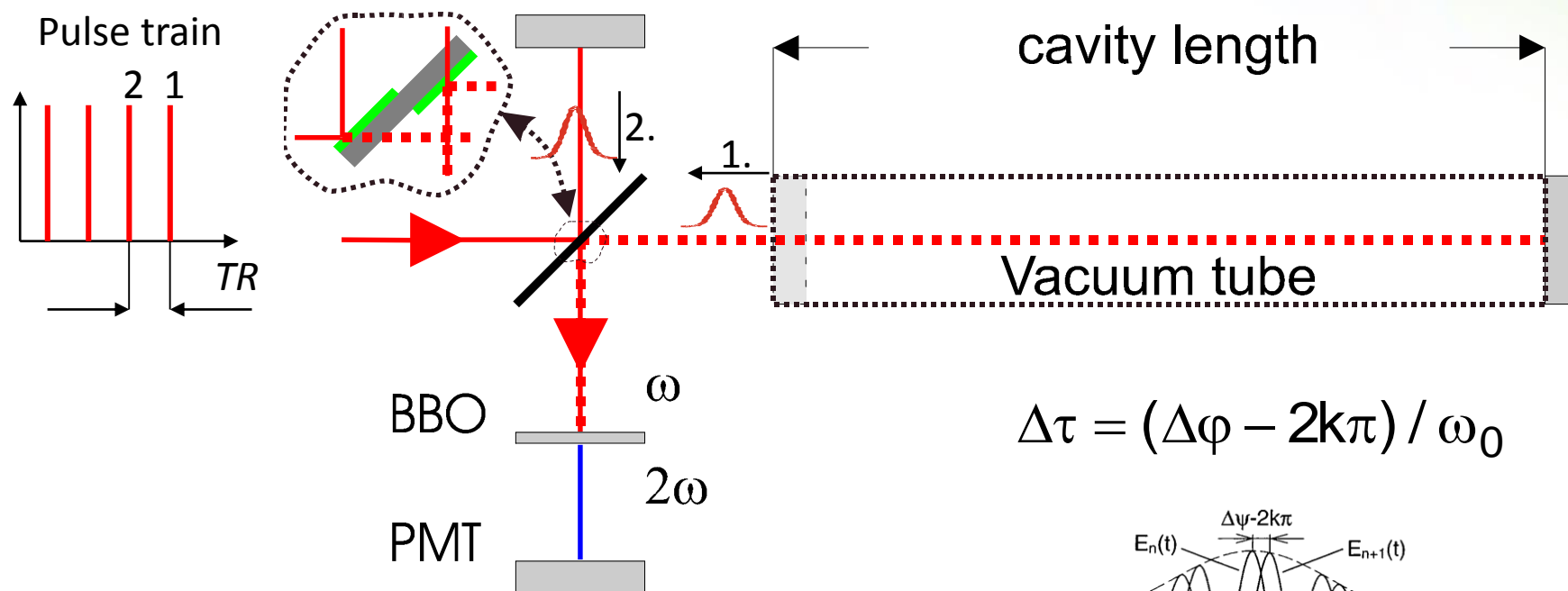
Getting hold of the comb offset: Different flavors of self-referencing

MEASURING CEP CHANGE

Can we measure the CEP change by linear means?

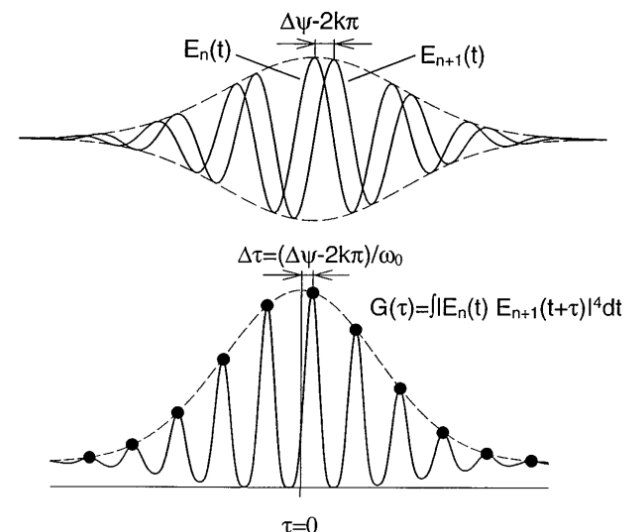


Earliest measurement (1996) did just this...



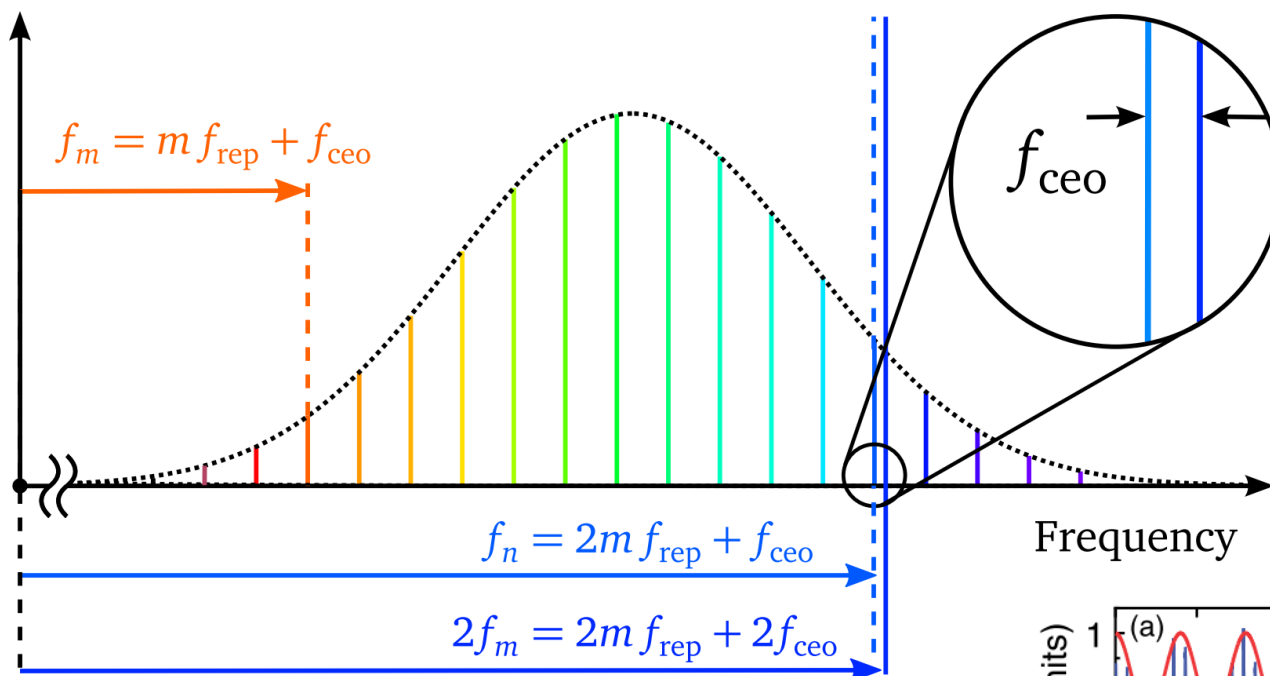
Results of this measurement:

- Value averaged over many ($>10^5$) pulses
- Showed dependency of $\Delta\Phi_{\text{ceo}}$ on
 - Intracavity dispersion
 - Pump power
- Low accuracy of only $\pi/10$



Detecting the offset frequency in time domain

Self-referencing scheme („f-to-2f“)



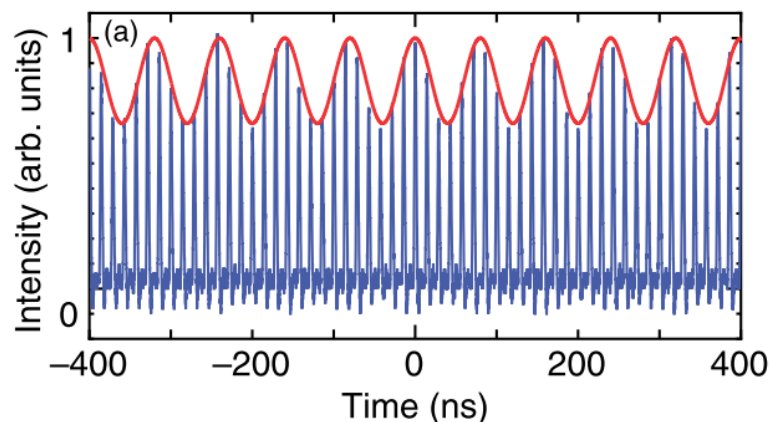
Interference of fundamental and SHG lines results in 'beating' at the difference frequency:

$$(f_n - 2f_m) \bmod f_{\text{rep}} = f_{\text{ceo}}$$

E. Reichert et al., Opt. Commun. **172**,59 (1999)
H. R. Telle et al., Appl. Phys. B **69**, 327 (1999)
D. J. Jones et al., Science **288**, 635 (2000)
A. Apolonski et al., Phys. Rev. Lett. **85**, 740 (2000)

Beat at spectral overlap:
 $(f_n - 2f_m) \bmod f_{\text{rep}} = f_{\text{ceo}}$

Pre-requisite:
Octave-spanning spectrum



Photodiode signal on oscilloscope

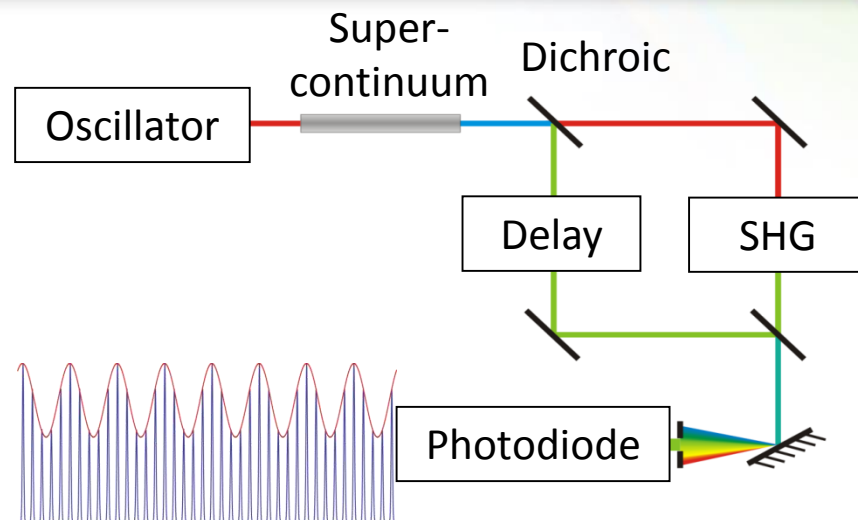
Mach-Zehnder “f-to-2f” type

Split-path “f-to-2f” interferometer (Michelson, Mach-Zehnder...)

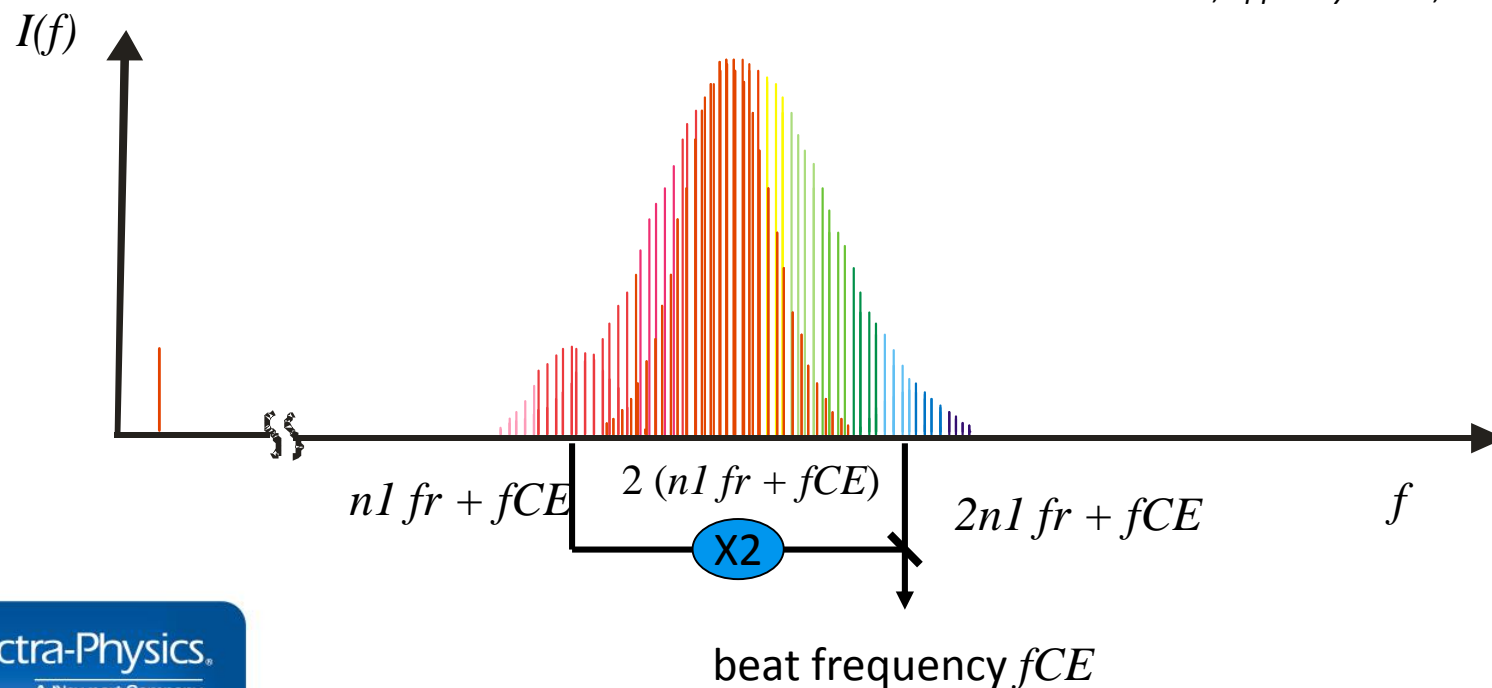
+ Applicable to long (<80 fs) pulses

– Various noise sources:

- Non-common paths
- Environment drifts
- Sensitive fiber coupling



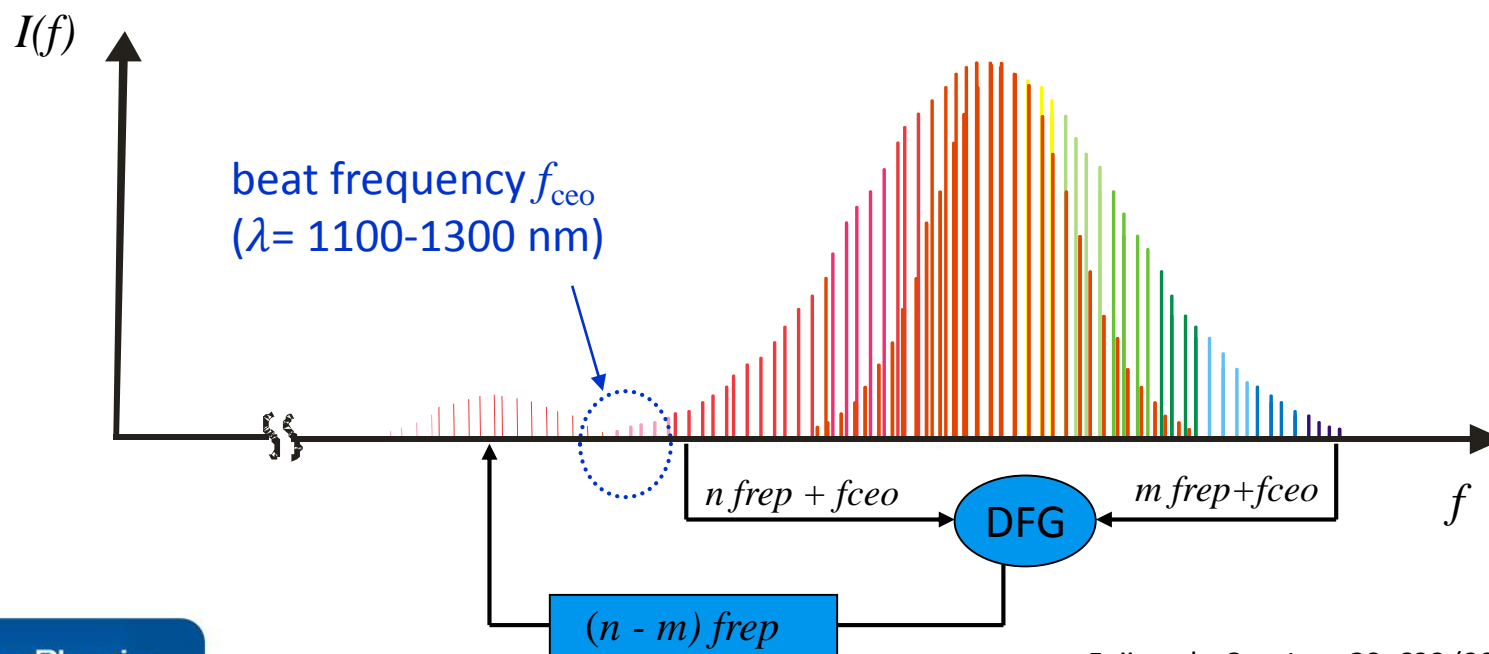
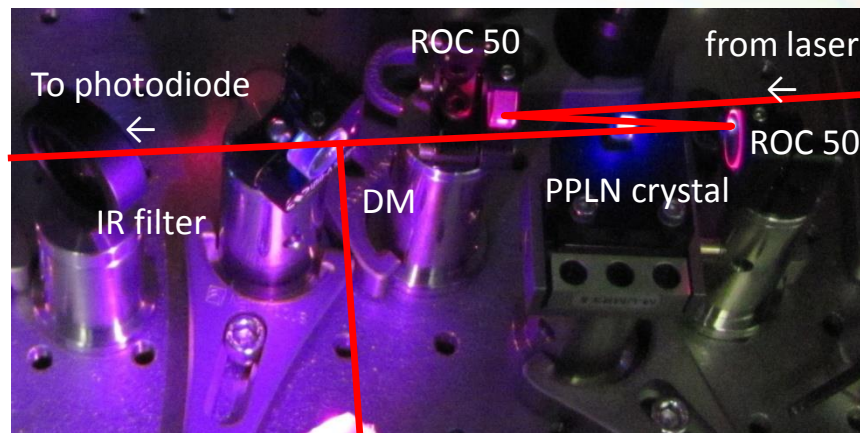
Telle et al., *Appl. Phys. B* **69**, 327 (1999)



Monolithic DFG “0-to-f” type

Monolithic “DFG” or “0-to-f” type

- + Robust and simple
- + Perfectly common-path
- + Set-and-forget device
- + Up to 45 dB S/N ratio
- + Insensitive to beam drift
- Requires compressed pulses with (almost) octave bandwidth

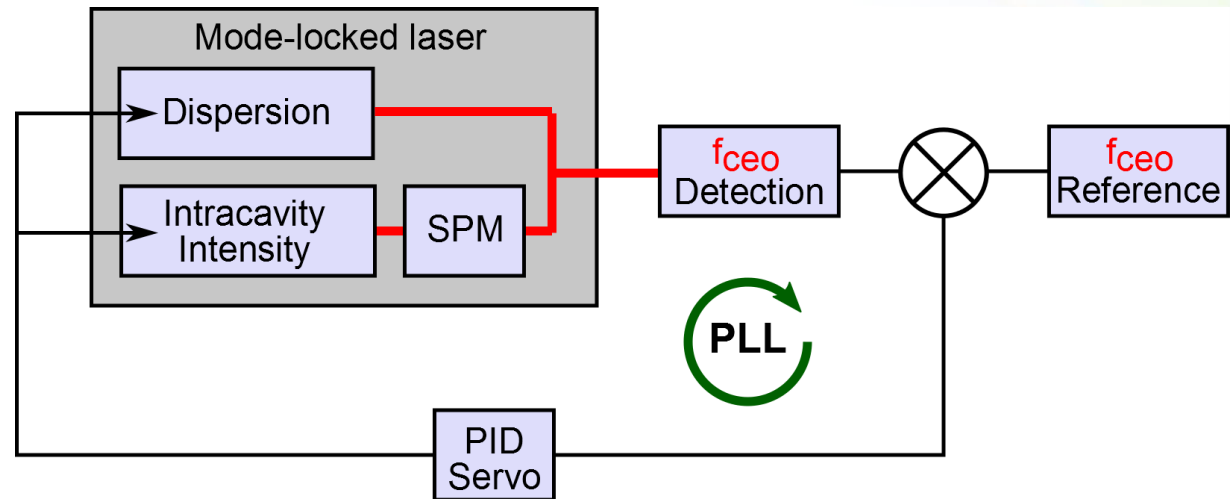


From random change to stable change: Fixing the comb offset

OSCILLATOR STABILIZATION

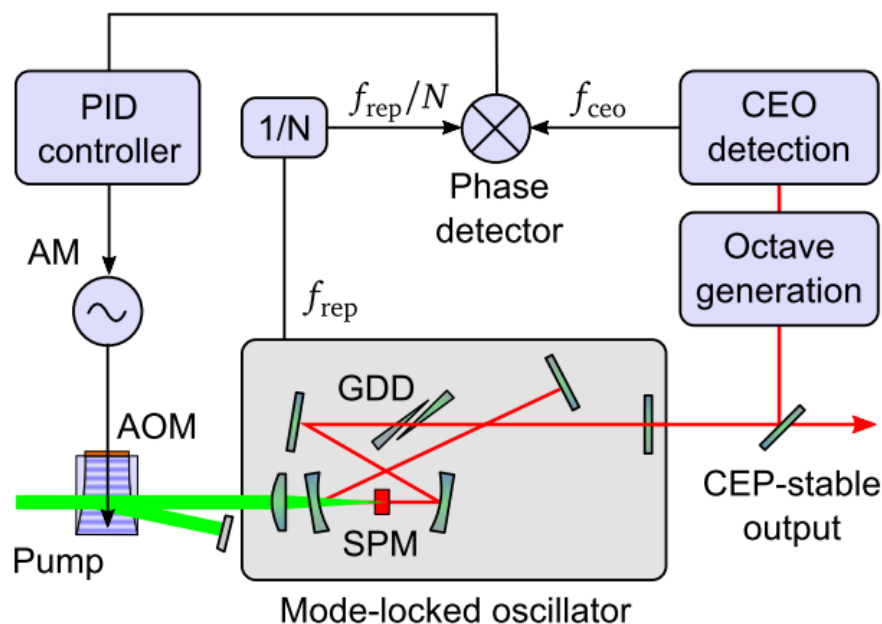
What handle to turn...?

...to change the pulse-to-pulse CEP change according to our wishes?



- Dispersion
 - Intracavity wedge insertion
 - End mirror tilting (beam path change through prisms)
 - Temperature changes in gain medium
- Intracavity intensity
 - End mirror tilt (also has impact on cavity Q)
 - Modulate gain (diode current, AOM in pump beam...)
 - Modulate loss (scattering AOM, graphene modulator, stimulated depletion...)
 - Polarization-dependent loss (EOM in fiber lasers, mostly)
- Frequency (center frequency directly linked to f_{ceo} !)

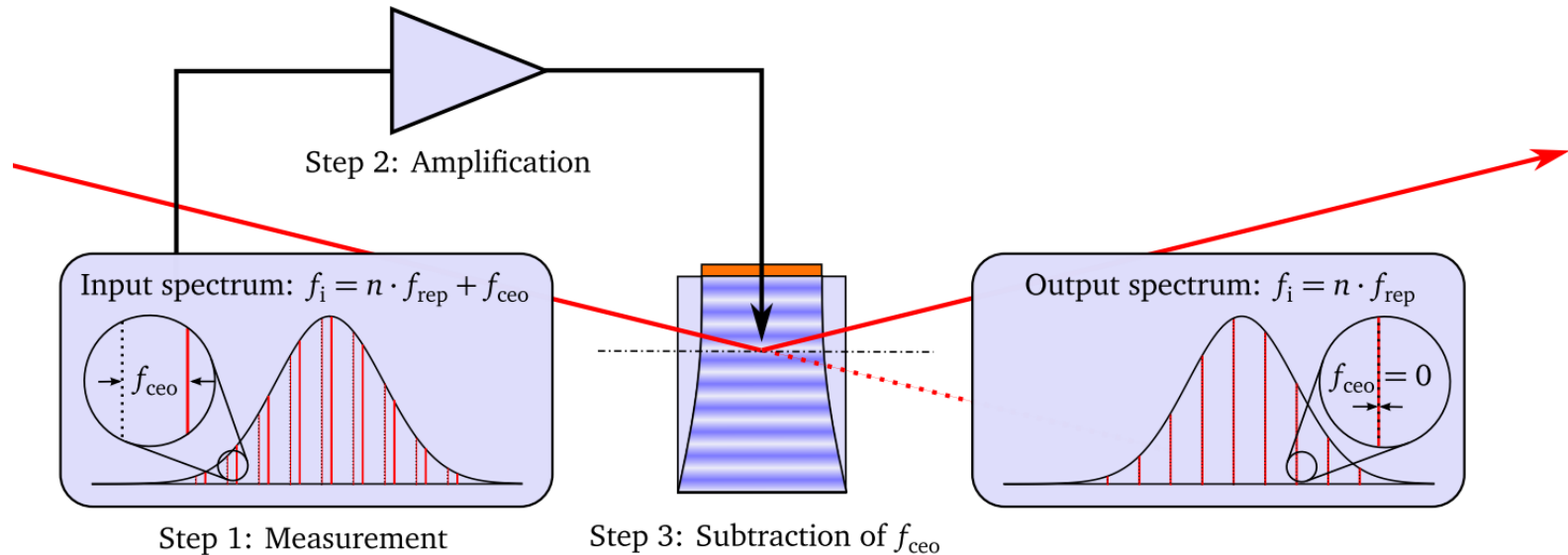
Ti:sa standard: Feed-back to pump power



- Earliest commercial approach for CEP stabilization
- Hours of CEP-stable operation when optimized for reliability
- Typical residual noise in Ti:sa oscillators: 90-180 mrad (optimized)
- Inherent drawbacks:
 - **Phase-lock loop trade-off:** Performance vs. Reliability
 - **Low correction bandwidth** (<100 kHz, typically 10-20 kHz)
 - $f_{\text{ceo}} = 0$ **impossible** with low-drift interferometers

Feed-forward* stabilization (CEP4)

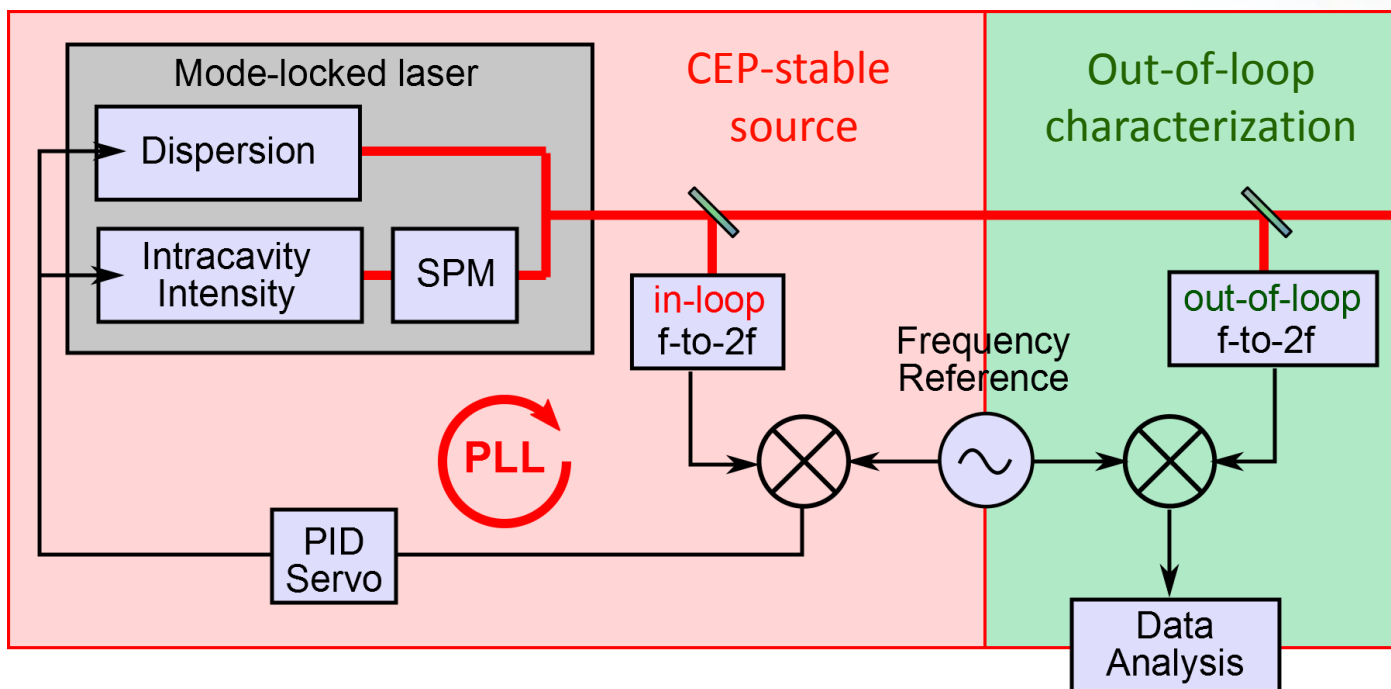
Idea: Shift the comb center frequency by just the right amount!



- + Never loses phase relation
- + Arbitrary CEO (simplest: $f_{\text{ceo}}=0$)
- + Control bandwidth >300 kHz independent of oscillator
- + Out-of-loop specs only

- Complications solved:
- Linear spatial chirp (use prism)
 - AOFS dispersion (use GDD mirrors)
 - Diffraction efficiency

Characterizing oscillator CEP properties



Any in-loop signal (e.g., the PID error signal) underestimates CEP noise!

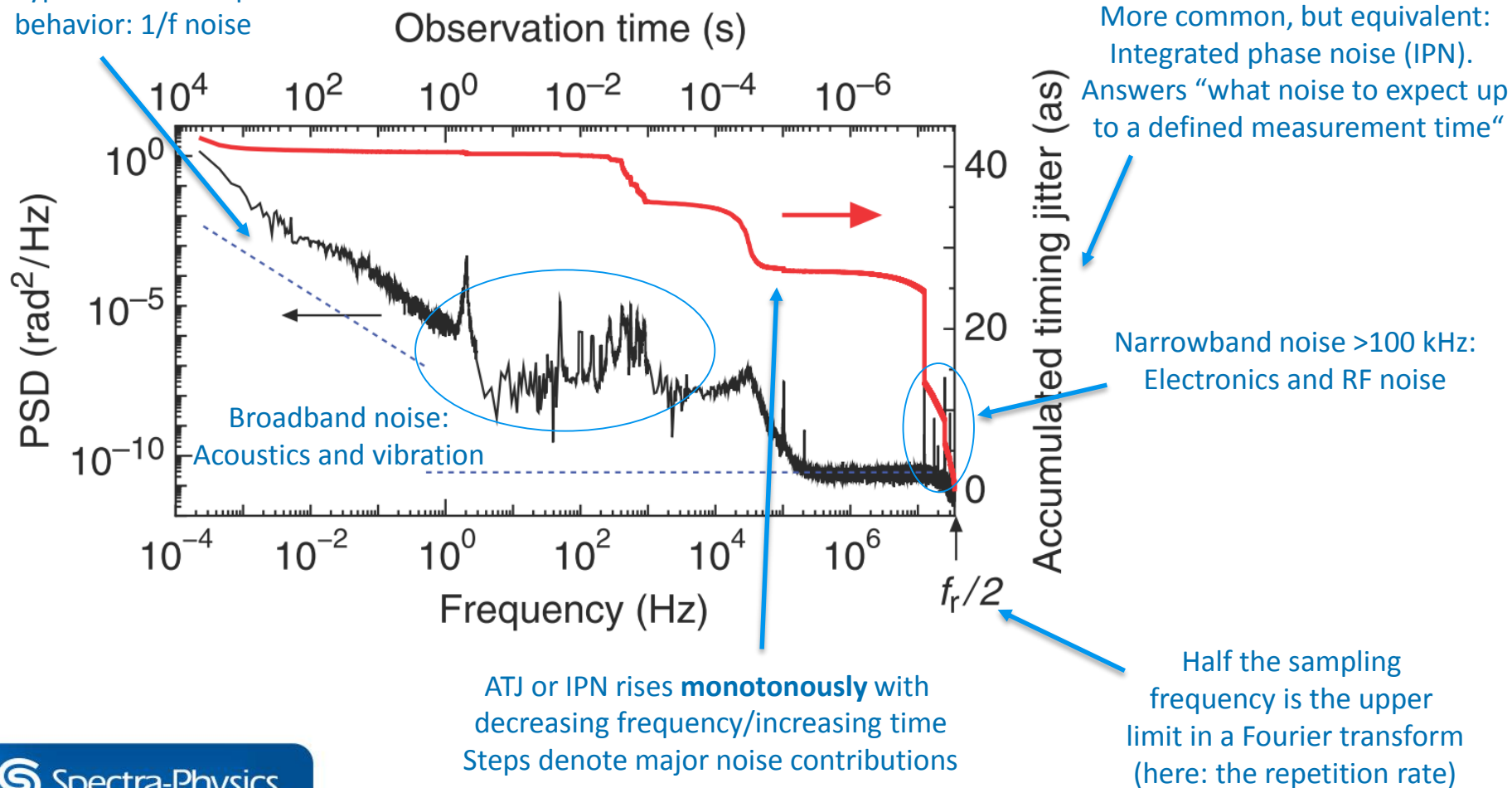
Proper method to measure the CEP performance of oscillators:

1. Lock f_{ceo} to a common reference (by whatever means)
2. Make a second (so-called out-of-loop) measurement of the stabilized output (f_{out})
3. Perform a phase comparison between the reference at f_{ref} and f_{out}
4. Record the suitably filtered signal and analyze...

Reading frequency-resolved noise plots

- Result of the measurement is the **phase error between f_{ref} and f_{out}**
- If this is properly sampled and calibrated, a Fourier transform leads to the plot below
- If f_{ceo} were set to 0, the phase noise figures here would correspond to the actual CEP

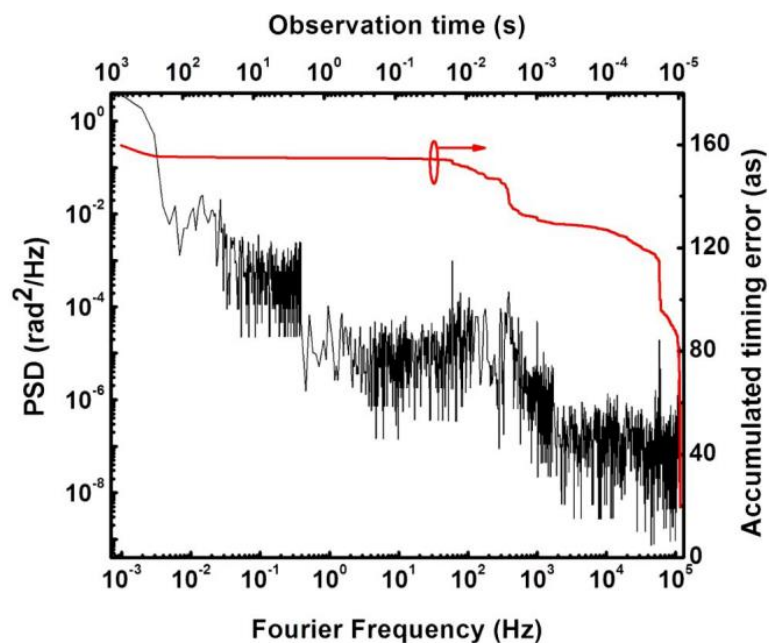
Typical out-of-loop
behavior: 1/f noise



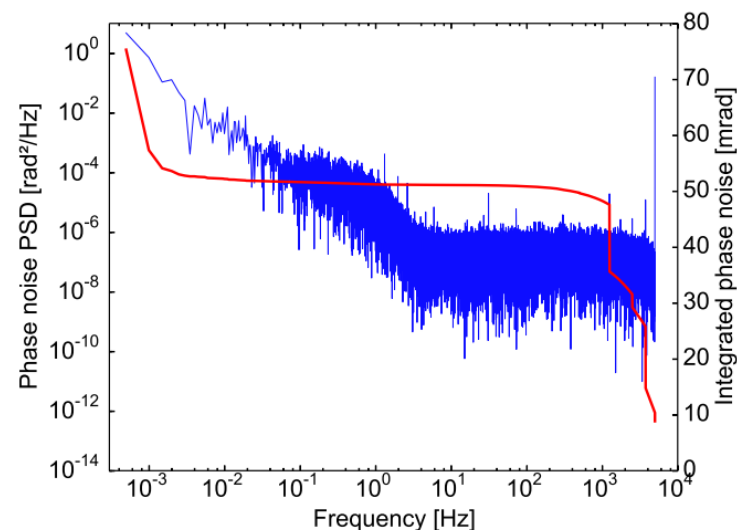
Some typical Ti:sapphire oscillator results

- Feed-back to pump power via AOM
- In-loop error signal
- 370 mrad (1 mHz – 102 kHz)

- Feed-forward to AOFS
- Out-of-loop measurement
- 80 mrad (0.5 mHz – 5 kHz)



Yun et al., *Applied Optics* **48**, 5127 (2009)



Lücking et al., *Optics Letters* **37**, 2076 (2012)

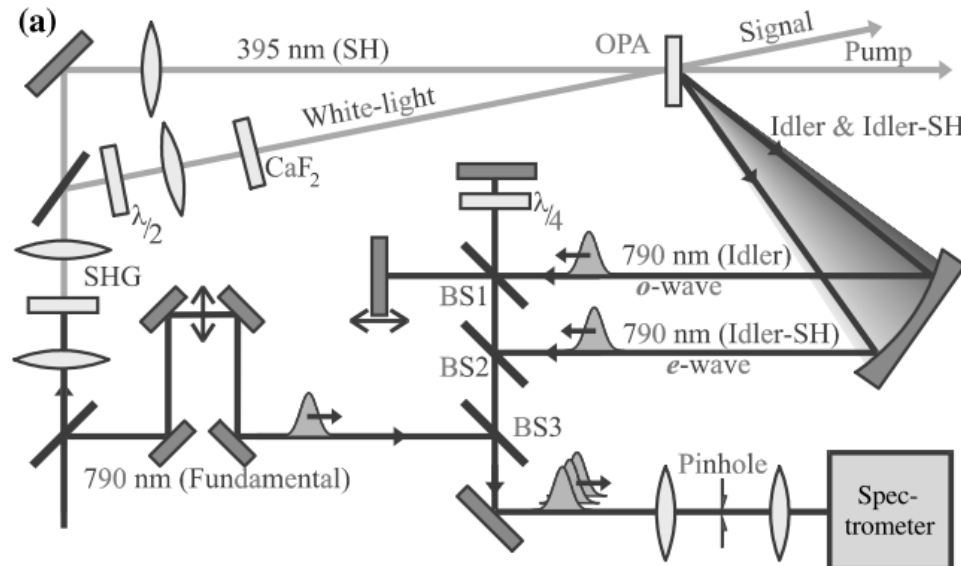
Passive stabilization via DFG

- During DFG/OPA, the idler carries the phase difference between pump and signal waves
- If those two are derived from the same source, the idler is “passively” CEP-stable

TABLE I. Phase properties of various OPA designs.

OPA configuration	A	B	C
Pump frequency, ω_P	ω_0	$2\omega_0$	$2\omega_0$
Central frequency of white light	ω_0	ω_0	$2\omega_0$
Phase offset of pump, ψ_P	ψ	$2\psi + \pi/2$	$2\psi + \pi/2$
Phase offset of signal, ψ_S	$\psi + \pi/2$	$\psi + \pi/2$	$2\psi + \pi$
Phase offset of idler, ψ_I	$-\pi$	$\psi - \pi/2$	$-\pi$
Self-stabilization of ψ_I ?	Yes	No	Yes

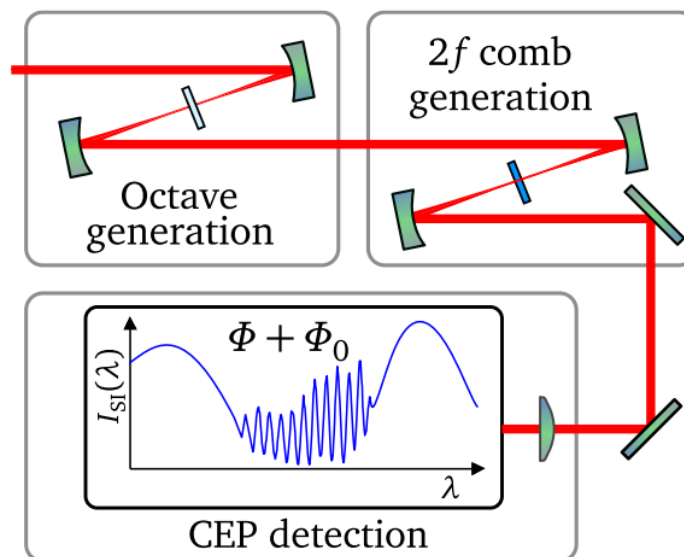
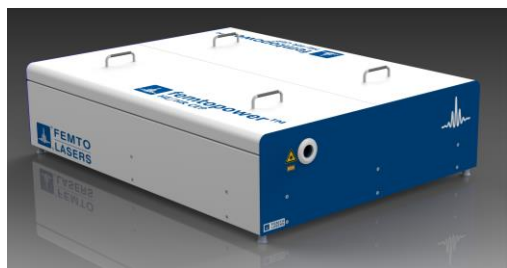
Baltuska et al., *Phys. Rev. Lett.* 88, 133901 (2002)



From nanojoule to millijoule

CEP STABILIZATION IN AMPLIFIERS

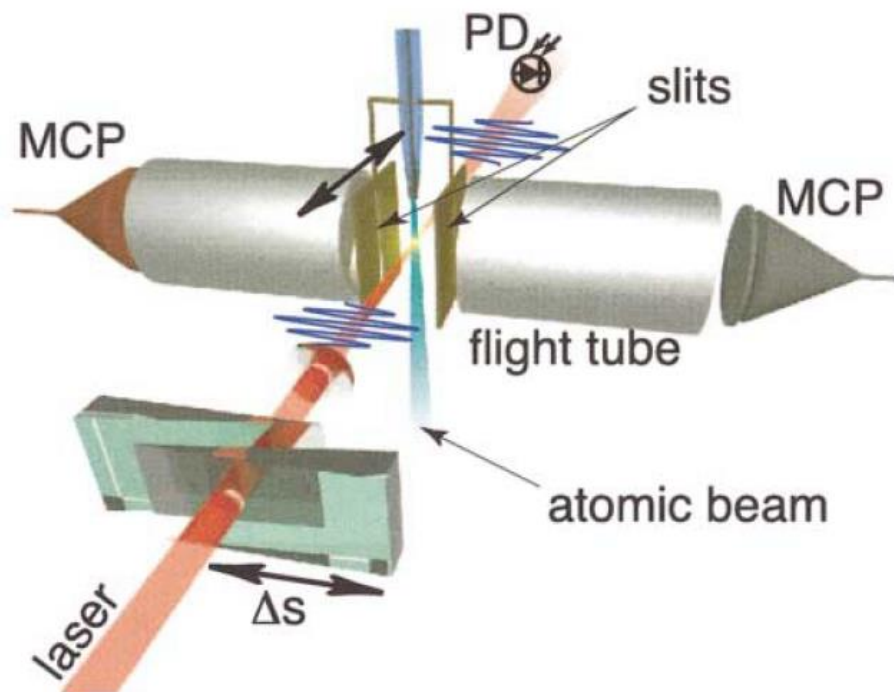
Single-pulse CEP from spectral interferometry



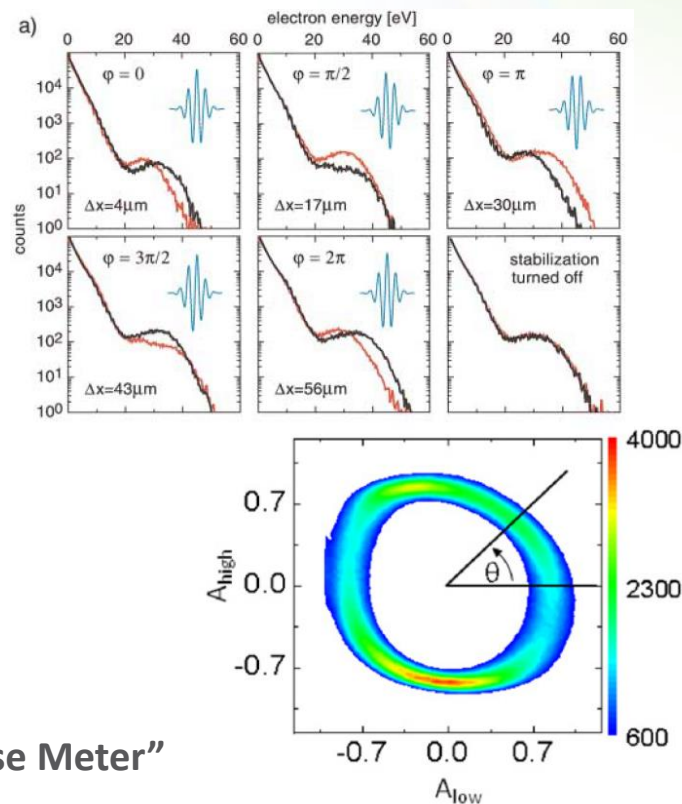
In-line (“collinear”) f-to-2f interferometer

- Self-referencing: Octave-spanning spectrum + SHG = Interference
- Interference fringes detected in spectral domain (using spectrometer)
- Fringe spacing corresponds to temporal delay between fundamental and SHG
- Fringe phase identical to CEP (+ unknown constant offset)
- Precision depends on energy noise, but typically 50-150 mrad
- Input energy: $<10 \mu\text{J}$
- Caution! Spectrometer must be set to acquire only single pulses!
To compare N -pulse averaging: Rms noise goes with $1/\sqrt{N}$...

Absolute CEP measurement with Stereo ATI



Stereo ATI, "CE Phase Meter"



- CEP is encoded in the energy spectra of left/right emitted ATI photoelectrons
- By choosing suitable energy ranges, the respective signal levels become parameters for a roughly spherical plot (PAP, "phase potato")
- Analog detection complex, but can be made fast (>10 kHz)
- Precision depends on pulse duration: <5 fs: 120 mrad, >12 fs: >350 mrad
- Required input energy between 35 and 175 μJ

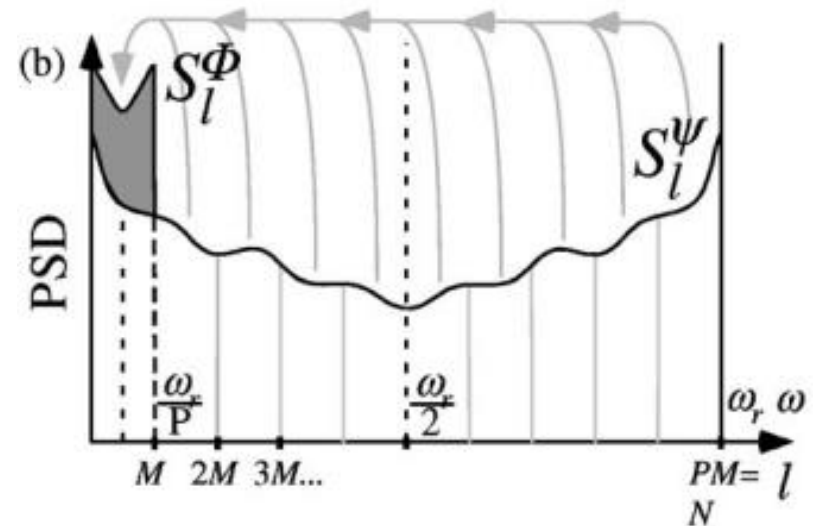
“Nyquist’s curse”

Nyquist frequency f_{Ny} : Half the sampling rate of a discrete-time system, $f_{Ny} = f_{sa}/2$

Shannon-Nyquist theorem:

“If a function $x(t)$ contains no frequencies higher than f_{Ny} , it is completely determined by giving its ordinates at a series of points spaced $1/(2f_{Ny})$ apart”.

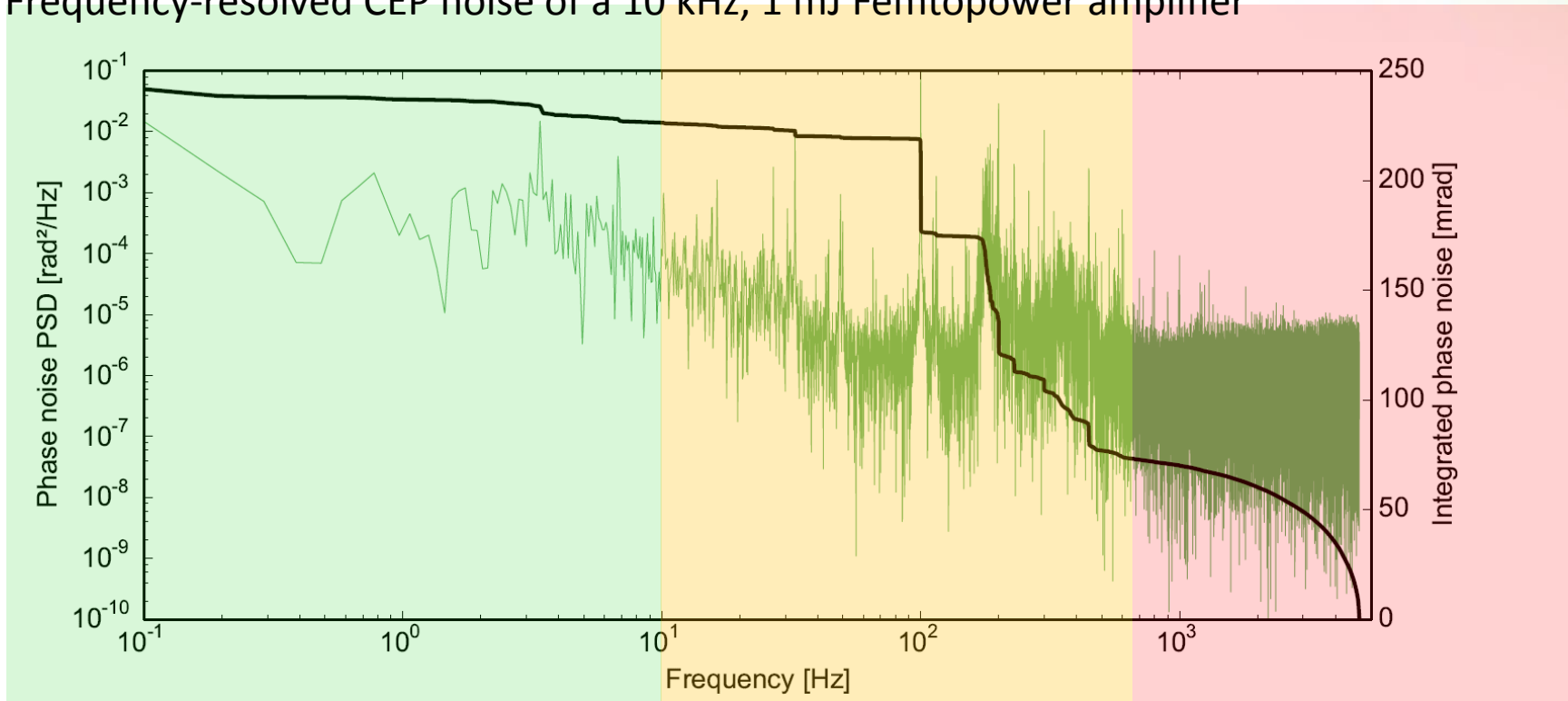
- Sampling CEP noise: Contributions can only be identified unambiguously when they occur at or below the Nyquist frequency.
- Start with a stabilized oscillator
 - repetition rate in the 10s of MHz range
- Amplifier sampling rate in the kHz range
 - subsampling by several 10^4
- What happens between to amplifier shots?



1. Whatever CEP noise accumulates between amplifier shots **can never be corrected!**
 - So start off with as low noise from the oscillator as possible
2. Correction of CEP noise from the amplifier **cannot be faster than half the sampling rate**
 - So measure as fast as possible – every single shot, at best!

CEP noise sources in amplifiers

Frequency-resolved CEP noise of a 10 kHz, 1 mJ Femtopower amplifier



Hz range and below:
Environmental drift
→ easily corrected

10 Hz – 1 kHz:
Acoustic range
→ **biggest contribution!**

> 1kHz:
f-to-2f noise floor
→ no correction possible

Keeping CEP noise low in amplifiers

f range	CEP noise sources in amplifiers:	Possible mitigations:
10–1000 Hz	<ul style="list-style-type: none">• Mechanical vibrations of large components<ul style="list-style-type: none">▪ Stretcher/Compressor (important!)▪ Mirror mounts	<ul style="list-style-type: none"><input type="checkbox"/> Avoid vibrations<ul style="list-style-type: none"><input type="checkbox"/> Use bulk stretcher<input type="checkbox"/> Low stretching factor<input type="checkbox"/> CEP detection >1 kHz and fast feed-back
>1000 Hz	<ul style="list-style-type: none">• Pump laser energy noise<ul style="list-style-type: none">▪ Stochastic (cannot cancel)	<ul style="list-style-type: none"><input type="checkbox"/> Low-noise pump laser<input type="checkbox"/> Saturate amplification
<10 Hz	<ul style="list-style-type: none">• Beam pointing drift, causing dispersion changes in stretcher/compressor	<ul style="list-style-type: none"><input type="checkbox"/> Stabilize separately

Lessons to learn from this...

1. Most noise comes from the acoustic range
2. Correction is difficult as it requires both a fast measurement and a fast actuator
3. Passive stability is paramount

CEP feed-back actuators in amplifiers

Offset in oscillator CEP locking loop (to pump power) Nature 421, 611 (2003); JSTQE 9, 972 (2003)

- ❑ Fast

- ❑ Two loops in comparable frequency ranges, same actuator: Unstable!

Introducing dispersion in some way

- Wedges/prisms in beam path Opt. Lett. 31, 3113 (2006)

- ❑ Slow (<100 Hz)

- Compressor grating separation or angle Appl. Phys. Lett. 92, 191114 (2008)

- ❑ Very slow (<10 Hz)

- ❑ Beam pointing impact

- ❑ All these: Dispersion impact on pulse duration

Acousto-optic devices

- AOPDF (“Dazzler”) Opt. Lett. 34, 1333 (2009)

- Fast (10 kHz)

- CEP4 AOFS grating phase Opt. Lett. 39, 3884 (2014)

- Simple add-on, no impact on any other parameter

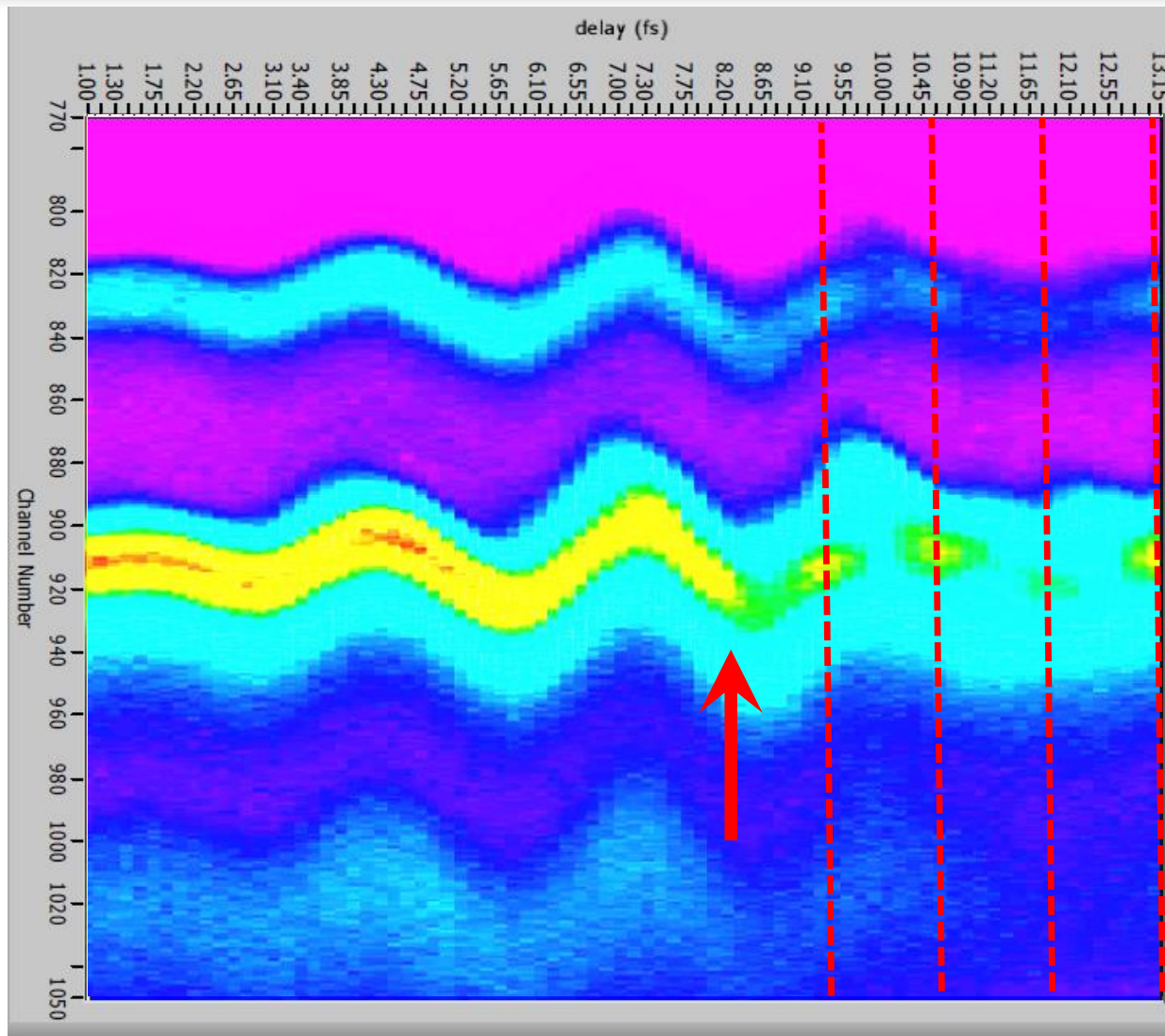
- Even faster (100 kHz)

- ❑ All these: No impact on pulse duration

How good is good enough?

HOT TOPICS AND CURRENT RESEARCH

CEP lock failure



PLL loses oscillator CEP lock around 8.2 fs delay:

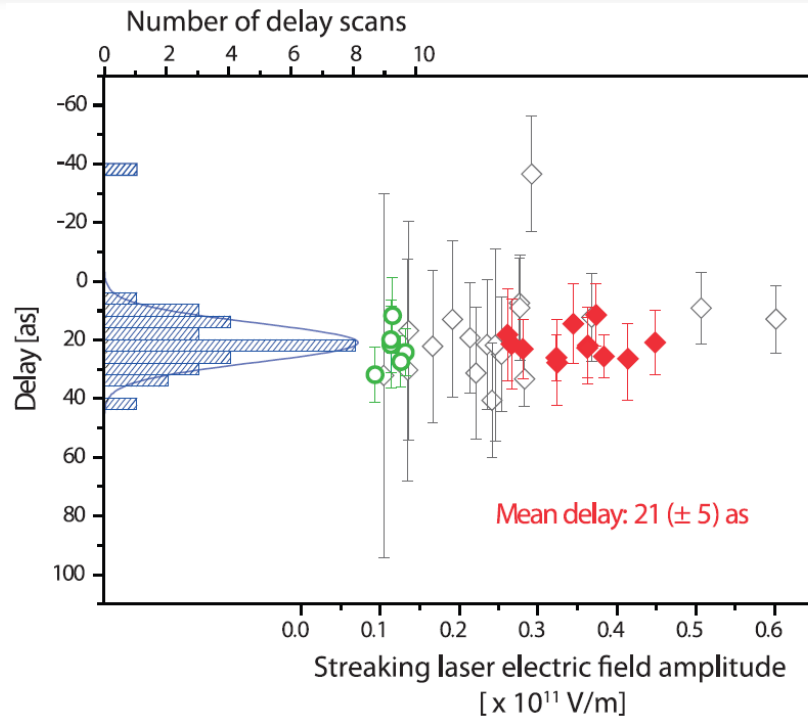
Re-lock possible, but **fixed phase relation is lost**

Random waveform drives attosecond pulse formation

Satellite pulses produce **modulation** of electron spectra

Caution:
f-to-2f interferometers might not even notice...

Challenges to CEP stabilization



“Synthesized Light Transients”, Wirth et al., Science 334 (2011):

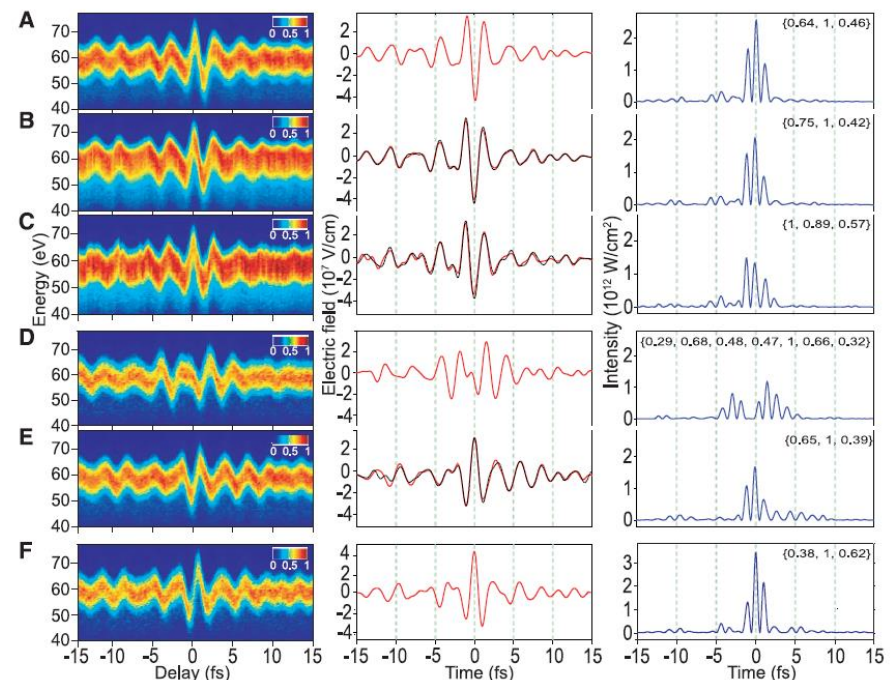
Sub-cycle NIR pulses as driving field for attosecond pulse generation

→ **Challenge #2: Precision**

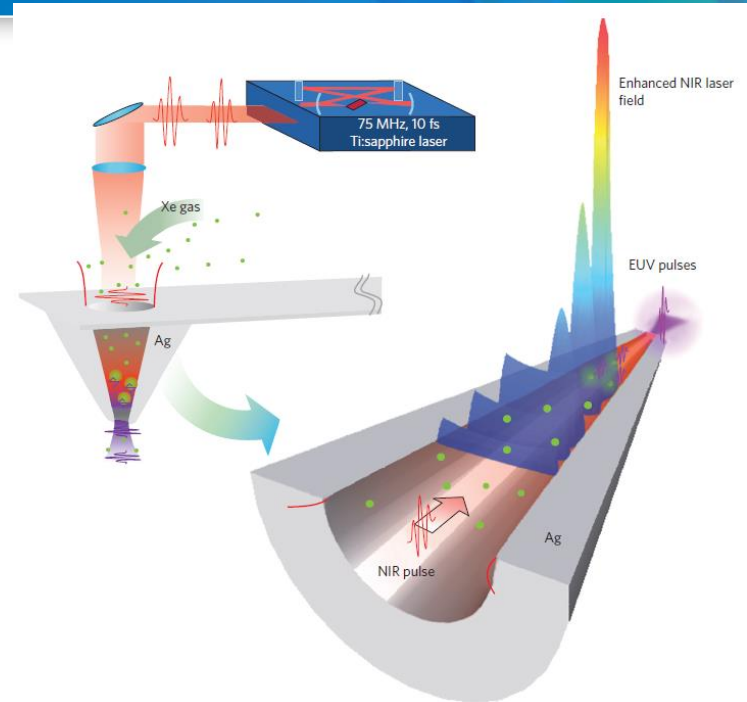
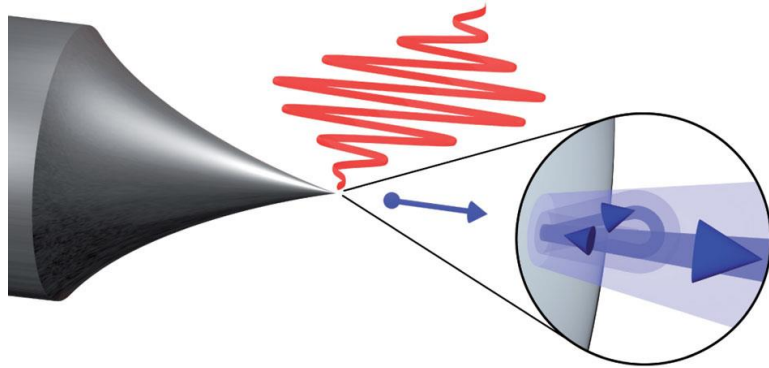
“Delay in Photoemission”, Schultze et al., Science 328 (2010)

Required tens of streaking spectrograms for dependable statistics – no lock failures
– no satellite pulses

→ **Challenge #1: Reliability**



Zero offset



Direct use of oscillators in attosecond science
Made possible by field enhancement, e.g.,

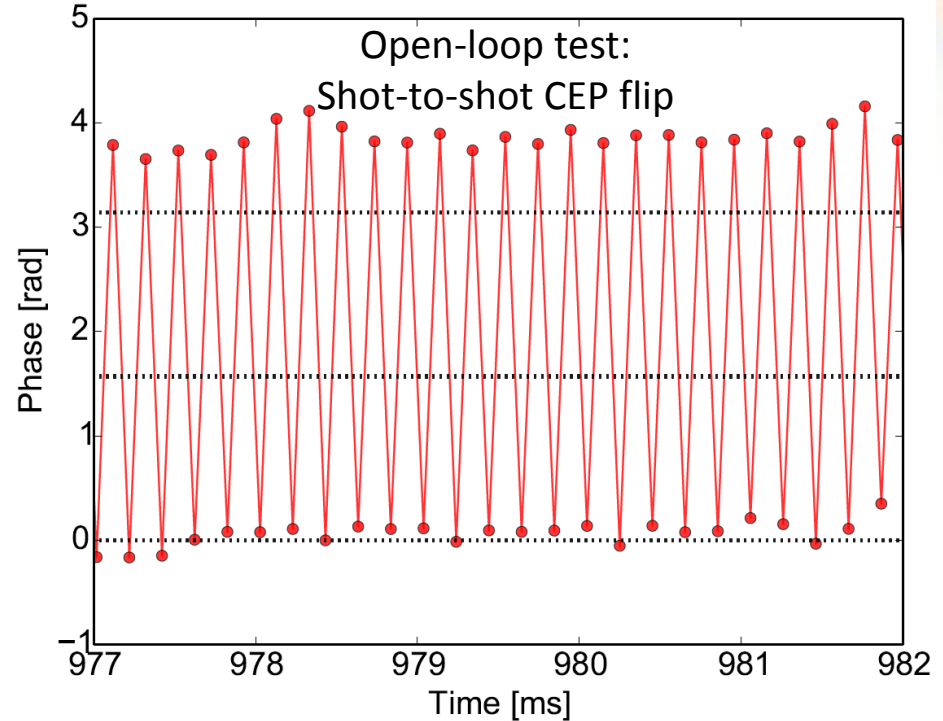
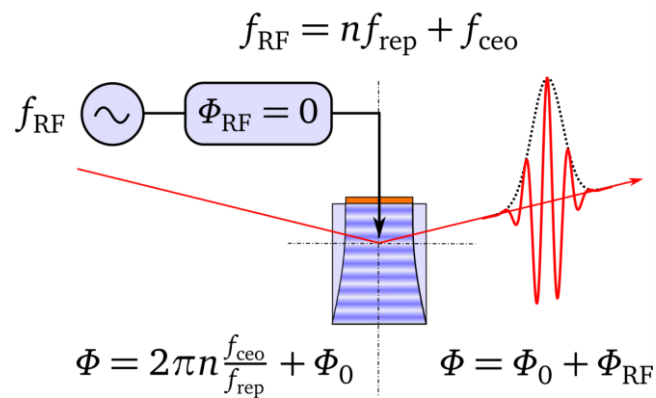
- At nanoscale metal tips [1], producing photocurrent modulation
- Using plasmonic waves on a conical surface [2] for high harmonic generation

Experiments require a train of **identical pulses at the full repetition rate**

- $f_{\text{ceo}} = 0$ – Hard to get with traditional stabilization
- **Seamless f_{ceo} scanning** – even harder...

→ **Challenge #3: Versatility**

Fast amplifier CEP correction using CEP4 phase



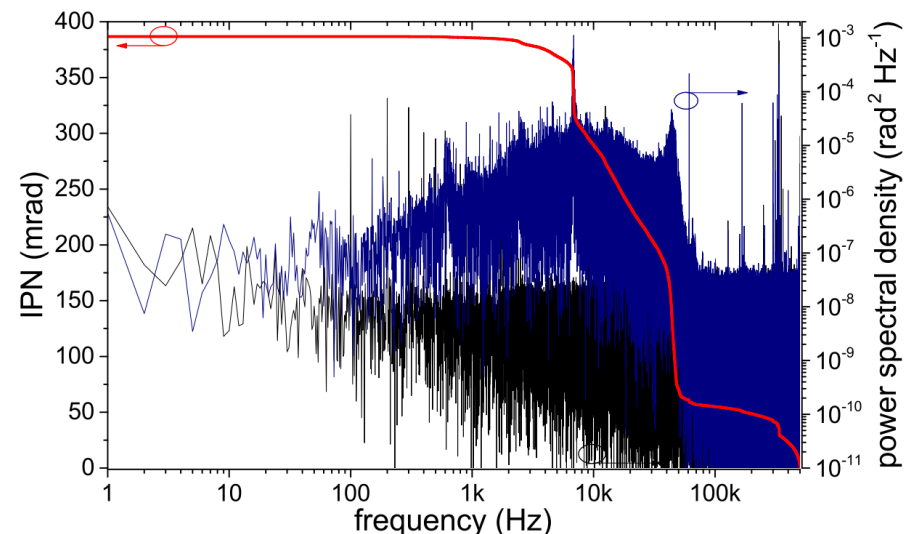
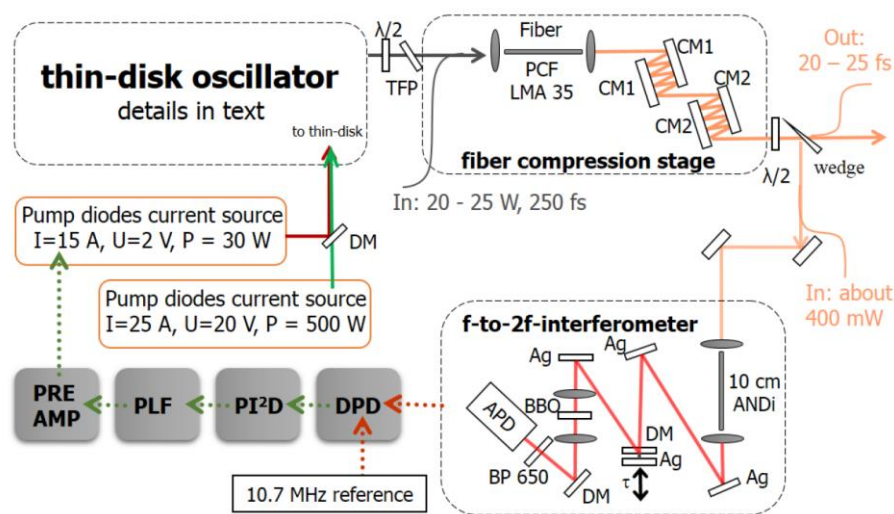
Frequency shifter:

RF frequency $\rightarrow \Delta\phi$ (CEP slip rate, set to zero)

RF phase $\rightarrow \phi$ (CEP itself)

- Acoustic grating phase is a free parameter in CEP4 stabilization
- Dispersion-independent, fast, easily added to existing systems
- > 100 kHz BW: Arbitrary CEP from shot to shot

Power scaling CEP-stable oscillators



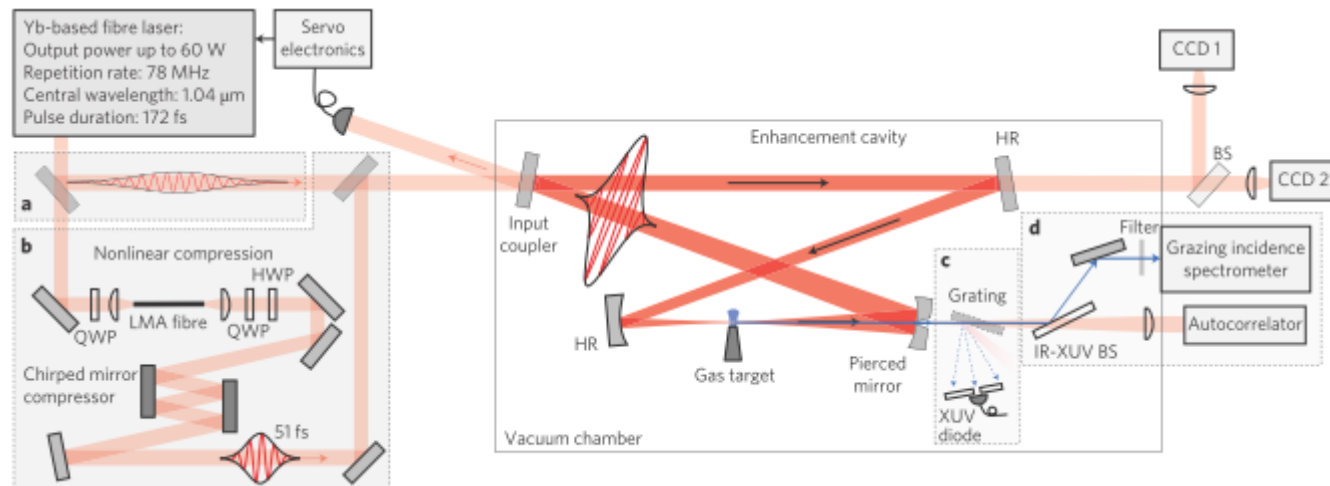
- Yb:YAG thin-disk hard to CEP-stabilize due to SBR issues
 - Overcome using hard-aperture Kerr lens mode-locking
- Compress pulses down to 10-20 fs
- CEP-stabilize using either scattering AOM [1] or second pump diode [2]
 - CEP noise comparable to early Ti:sapphire oscillators

[1] Pronin et al., "High-power multi-megahertz source of waveform-stabilized few-cycle light," Nature Communications 6, 6988 (2015)

[2] Seidel et al., "Carrier-envelope-phase stabilization via dual wavelength pumping," Opt. Lett. (in print, 2016)

Enhancement cavities

- HHG with its low efficiency lends itself to cavity enhancement
- Groups at Munich (bulk/fiber hybrid) and Jena (fibers) are pushing in this direction
- Enhancement of <30 fs pulses requires full frequency comb stabilization

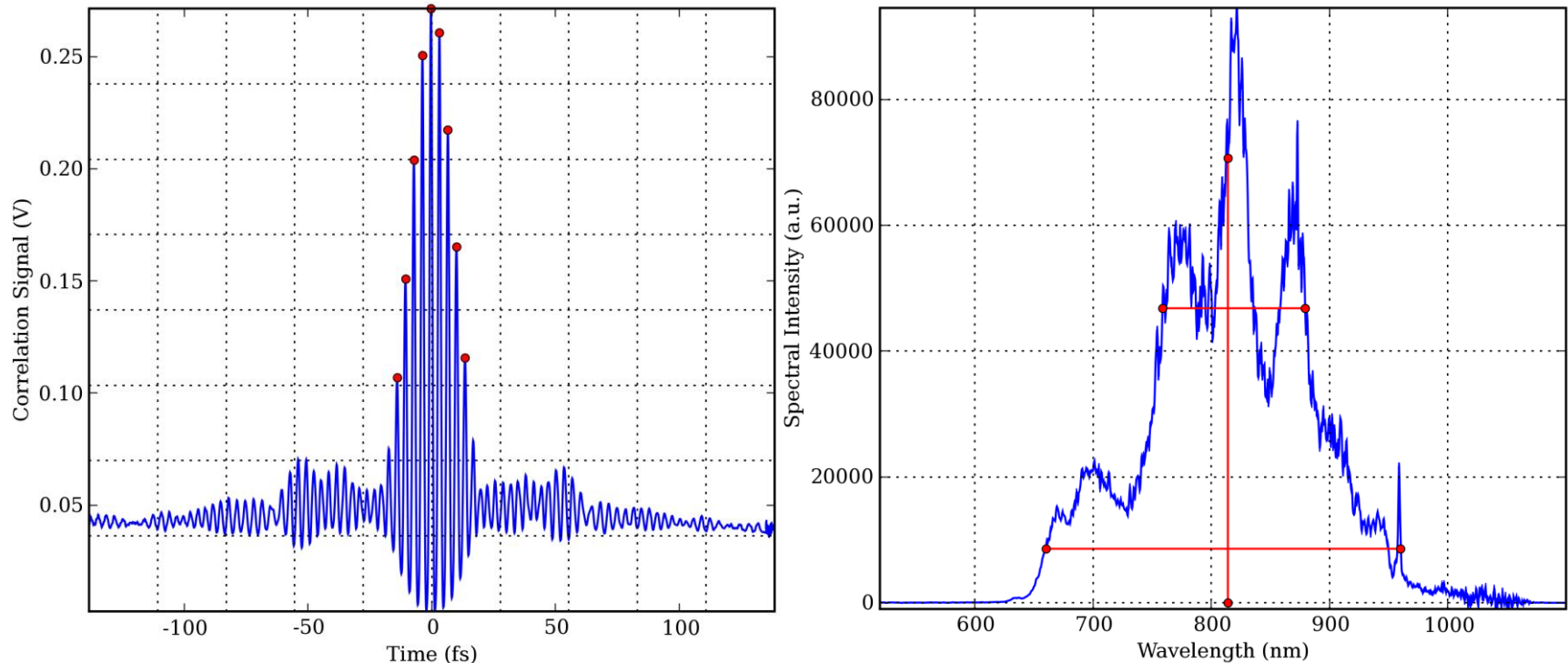


Thank you for your attention!

QUESTIONS?

ADDITIONAL MATERIAL

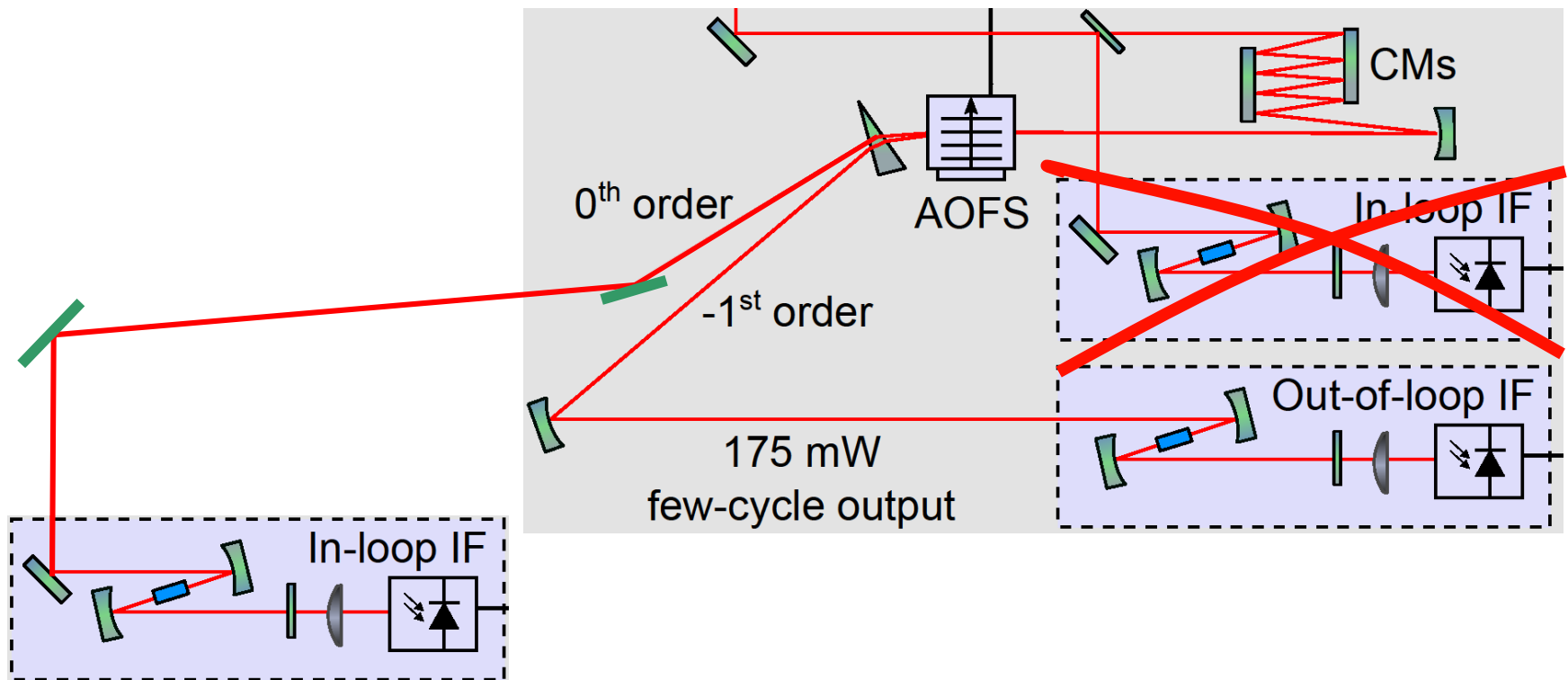
CEP 4: Autocorrelation after AOFS and wedge



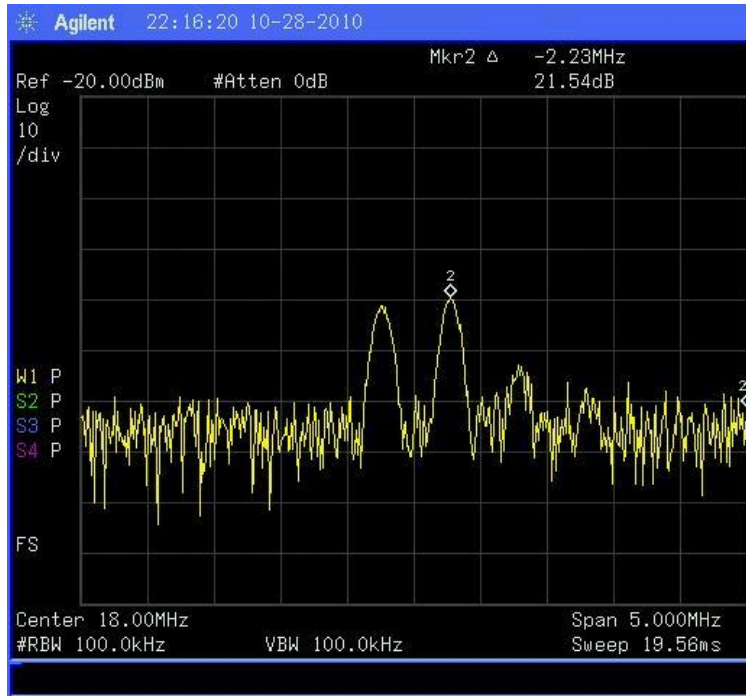
- Measured after wedge and collimating mirror in -1st order
- Fringe-resolved SHG autocorrelation yields 9.8 fs pulse duration
- Fourier limit: <7 fs
- Recompression limited by mirrors: Better TOD match possible

0th order in-loop detection

- Why not use 0th order power for in-loop measurement?
- Worked fine in fiber-based experiment...



0th order in-loop detection



But: In-loop f_{CE} signal behaves strange:

- FF loop open: f_{CE} signal fine
- FF loop gradually closing:
Sidebands appear in RF spectrum
- Sidebands are equidistant at some 300-900 kHz, depending on AOFS alignment...

- Problem: SNR in monolithic 0-to-f is extremely power-dependent
- We introduced a feedback loop that oscillates at its resonance...

Measured “by accident”:

Control bandwidth of FF scheme: >300 kHz

f-noise to Φ -noise

$$\frac{\Delta\varphi}{T}$$

: f_{CE} phase error over measurement time T

$$f_{CE,lin} = f_{CE} + \frac{\Delta\varphi}{2\pi T}$$

: Corresponding frequency shift over measurement time

$$\Delta\Phi = 2\pi \frac{f_{CE}}{f_{rep}}$$

: Pulse-to-pulse CEP shift

$$\Delta\Phi(t) = 2\pi \frac{f_{CE}}{f_{rep}} \cdot \frac{t}{T_{RT}} = 2\pi t f_{CE}$$

: Accumulated CEP over time t assuming no error

$$= 2\pi t \left(f_{CE} + \frac{\Delta\varphi}{2\pi T} \right)$$

: Accumulated CEP over time t with linearized error

$$= \frac{\Delta\varphi}{T} t$$

: Accumulated CEP over time t with $f_{CE}=0$

$$\Delta\Phi = \Delta\varphi$$

: Accumulated CEP over measurement time with $f_{CE}=0$